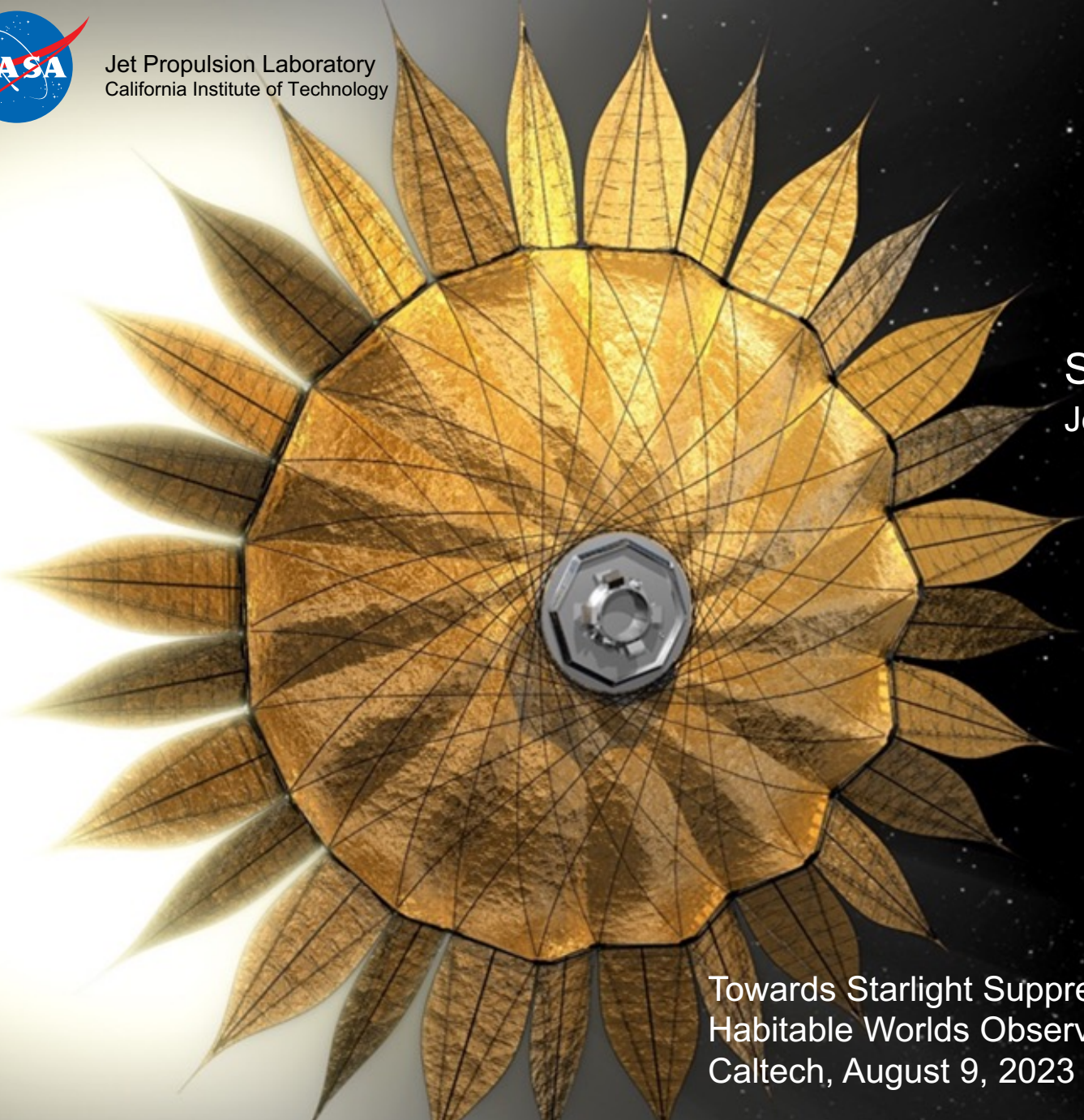


Jet Propulsion Laboratory  
California Institute of Technology

# STARSHADE ATTRIBUTES

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Jet Propulsion Laboratory, California Institute of Technology



Towards Starlight Suppression for the  
Habitable Worlds Observatory Workshop  
Caltech, August 9, 2023

# WHY STARSHADES?

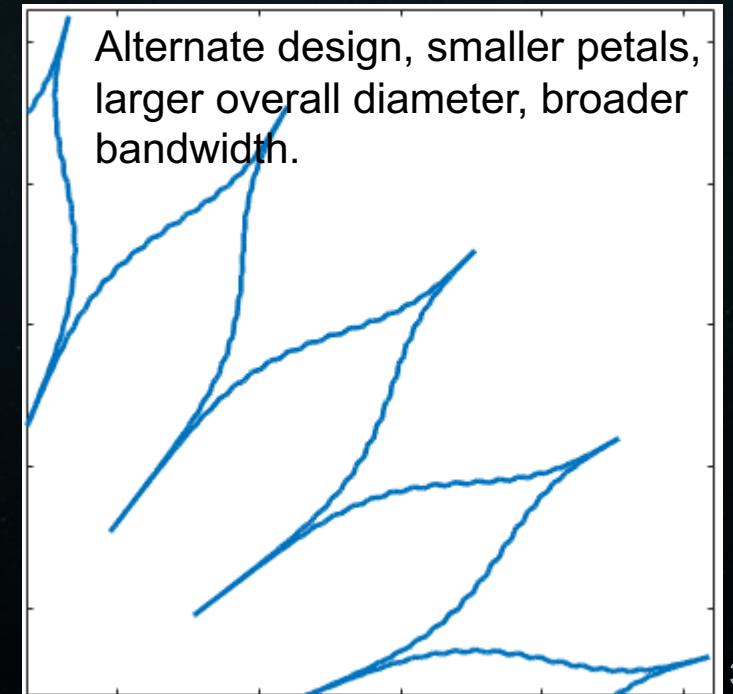
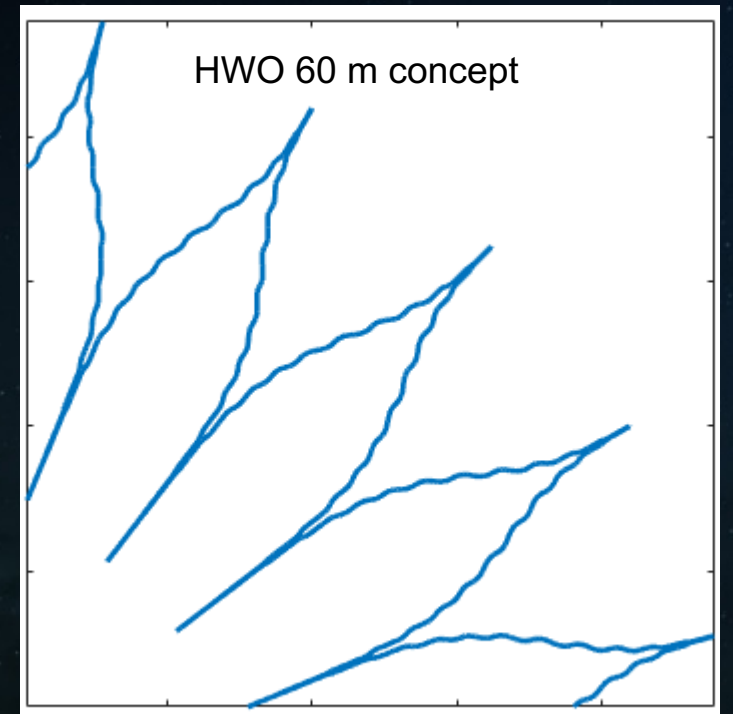
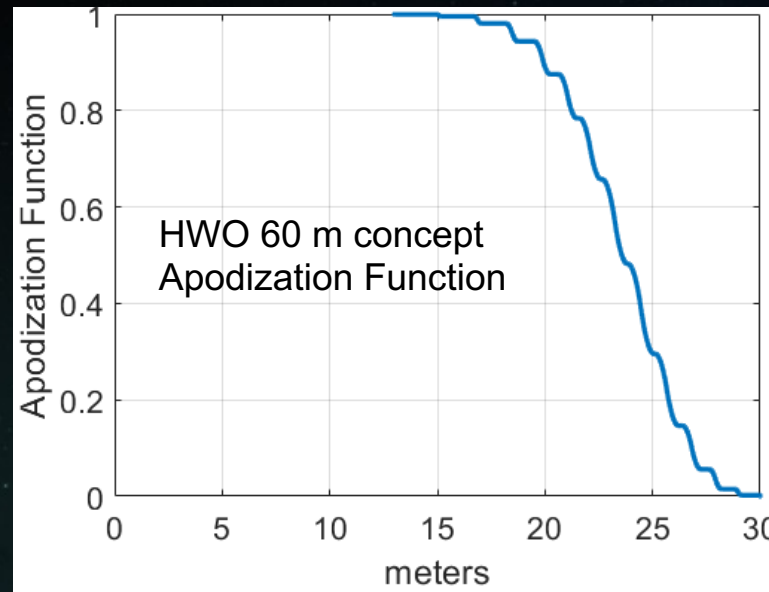
*Starshades remove the starlight **before** it can scatter into the telescope.*

| Parameter                                   | HWO 60-m Starshade concept  | Demonstrated             |
|---|---|--------------------------|
| IWA   | >1.89 $\lambda/D$   | 1.8 $\lambda/D$          |
| OWA   | Unlimited   | 3.6 $\lambda/D$          |
| Bandwidth                                   | 67%   | 12.5%                    |
| Instrument Contrast                         | < 4e-11   | <1e-10 (75% search area) |
| Throughput                                  | 100%  | 90%                      |
| Telescope stability,<br>shape, segmentation | Works equally well with any<br>aperture:<br>on- or off-axis,<br>segmented or monolith,<br>does not drive stability,<br>does not drive coating uniformity. | Circular aperture        |



# SHAPE

- Flower-like shape is binary approximation to a smooth apodization function.
  - Required for deep contrast and a wide shadow.
  - Balance IWA, shadow size, starshade diameter
- Optimization tools (e.g. Cady et al, Opt. Express 2010) let us design for:
  - Minimum diameter for a given IWA, bandpass, and shadow size
  - Accommodate for engineering constraints:
    - Petal length, petal tip width, petal gap width
- HWO concept parameters:
  - Tip width: 16 mm
  - Gap width: 2.1 mm
  - Petal length: 16 m
  - Disk Diameter: 28 m



**Design tool has been validated  
at 1e-10 contrast in the Princeton  
Starshade Testbed.**

# SIZE: EXAMPLES

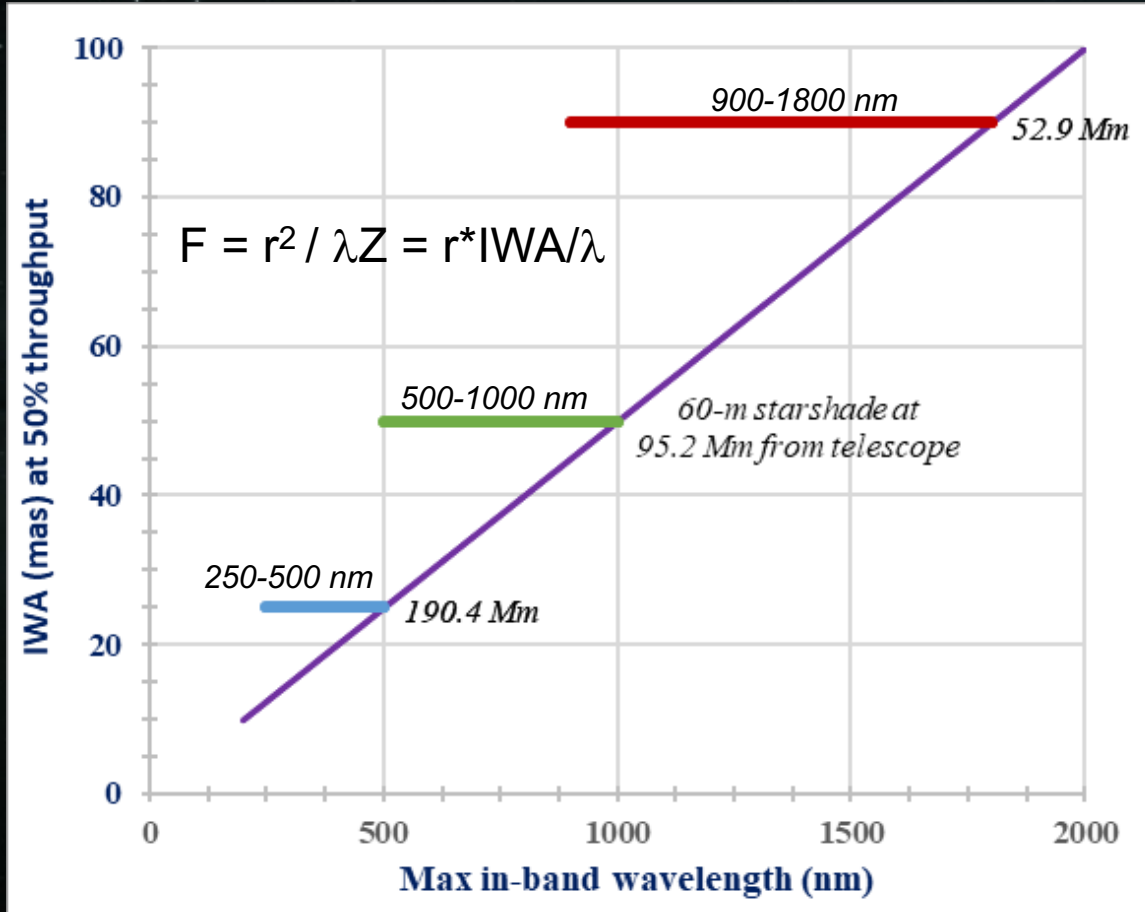
| Telescope               | Tel. Diam. (m) | Bandpass (nm) | IWA (mas)<br>Tip / 50% | Starshade Diam.<br>(tip to tip, m) |
|-------------------------|----------------|---------------|------------------------|------------------------------------|
| HWO                     | 6              | 500-1000      | 65 / 51                | 60                                 |
| HWO (UV)                | 6              | 225-500       | 65 / 51                | 35                                 |
| HabEx                   | 4              | 300-1000      | 70 / 58                | 52                                 |
| Roman<br>Rendezvous     | 2.4            | 615-800       | 104 / 85               | 26                                 |
| Occulting<br>Ozone Obs. | 0.6-1.5        | 200-500       | 103/85                 | 16                                 |

Starshade diameter scales more slowly than telescope diameter.  
The HWO concept starshade has a diameter of 60 m and an  $IWA_{\text{tip}}$  of 65 mas.

# BANDPASS AND IWA

The same starshade can be used at ANY maximum wavelength. The IWA scales with wavelength.

HWO 60 m starshade IWA (tip) and Separation



HWO 60 m starshade IWA and Separation

| Bandpass (nm) | IWA (mas) Tip / 50% | Distance (Mm) |
|---------------|---------------------|---------------|
| 250-500       | 32.5 / 43           | 190.4         |
| 500-1000      | 65 / 51             | 95.2          |
| 900-1800      | 117 / 92            | 47.6          |

HWO 35 m starshade IWA and Separation

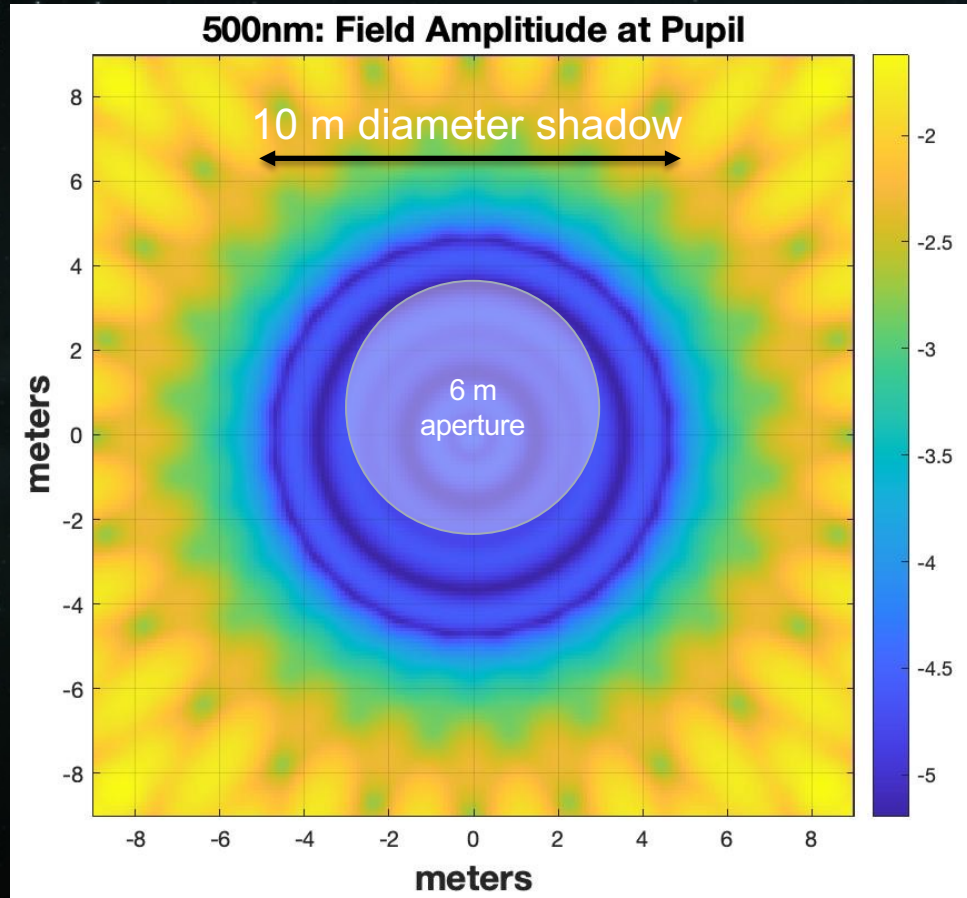
| Bandpass (nm) | IWA (mas) Tip / 50% | Distance (Mm) |
|---------------|---------------------|---------------|
| 225-500       | 65 / 51             | 55.5          |
| 338-750       | 97.5 / 76           | 37.0          |
| 450-1000      | 130 / 102           | 27.8          |

For the 60 m,  $IWA_{tip}$  is at  $1.89 \lambda/D$ .  
For the 35 m,  $IWA_{0.5}$  is  $3.0 \lambda/D$ .



# FLYING IN THE SHADOW

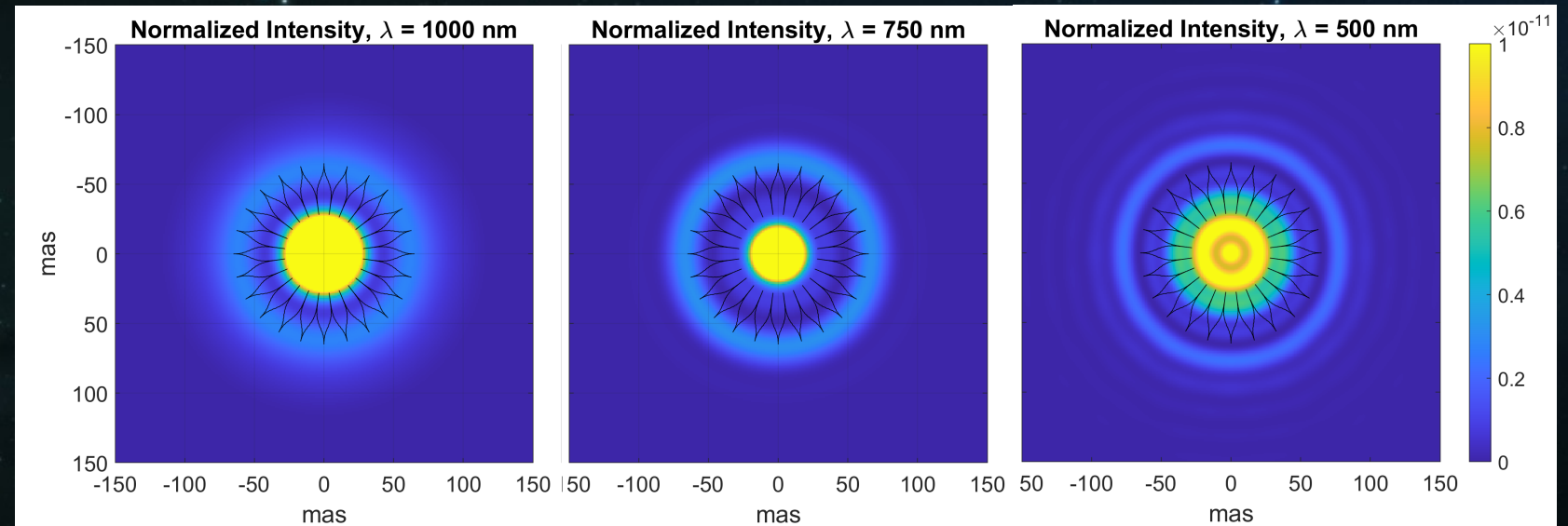
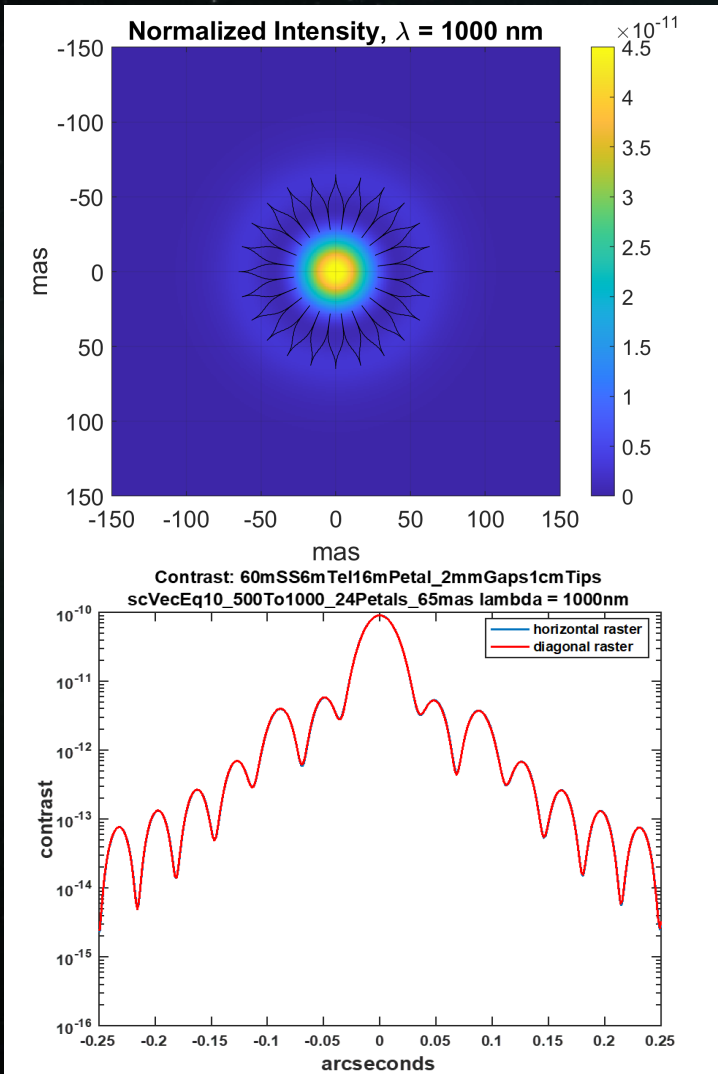
The shadow is designed to be larger than the telescope pupil to allow for lateral motion. For the HWO concept, we designed the shadow to be 10 m in diameter, for a  $\pm 2$  m radial tolerance.



With a  $\pm 2$  m radial tolerance, the sensing requirement is significantly relaxed compared to laboratory results, and the formation control bandwidth is  $\sim 600$  s.

# CONTRAST (STARLIGHT LEAKAGE)

Starshade designs with reasonable engineering constraints will perform better than  $1e-10$ . Here are the diffraction patterns for the HWO 60 m starshade (the as designed shape, no perturbations).



The design contrast at  $IWA_{tip}$  is  $\sim 5e-12$ . In practice, with lab-proven tolerancing, the instrument contrast at the IWA will be  $\sim 4e-11$ .

Contrast improves with working angle, ringing down to nearly zero at 150 mas. There is no outer working angle limitation.

# BANDWIDTH

A finite bandpass is desirable because the bright light leaking on either side of the suppression band can be used for formation flying.

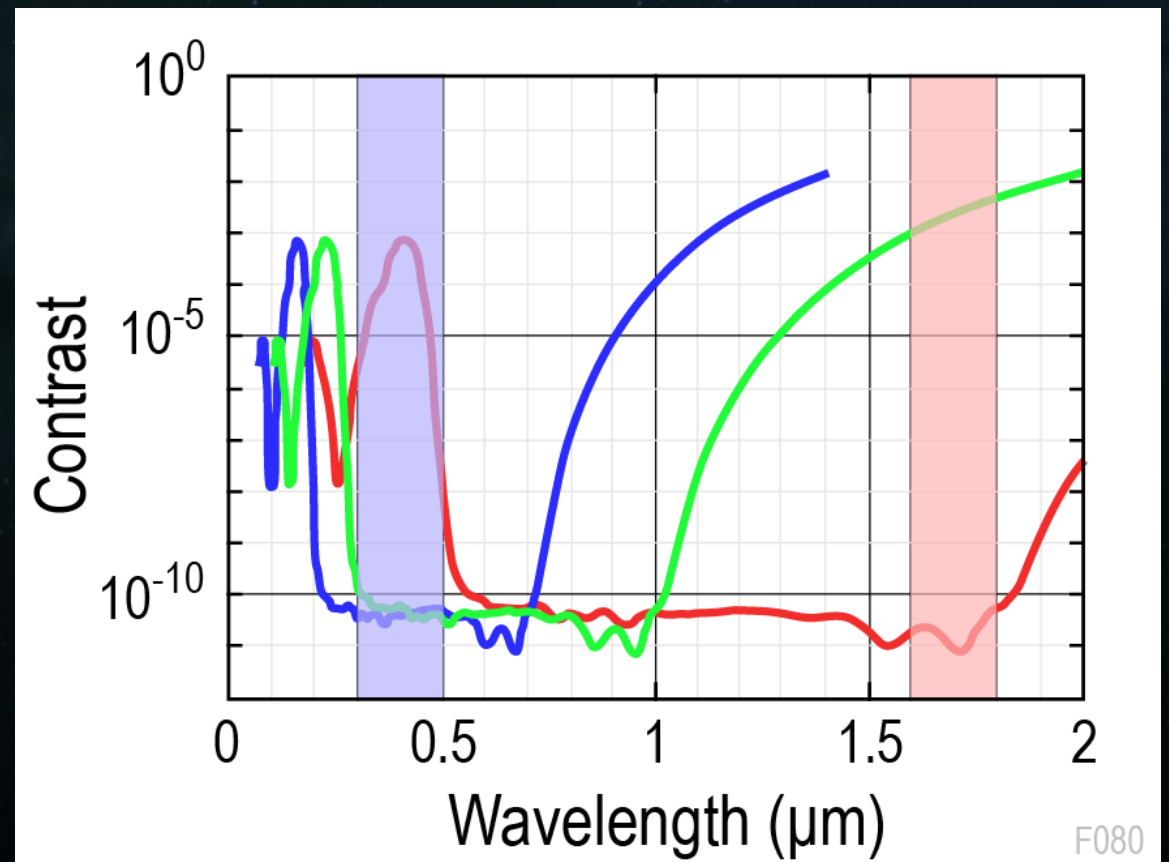
We use HabEx as an example. HWO will be similar.

When positioned for the visible band (green line), the red box 1.6-1.8  $\mu\text{m}$  provides the formation flying signal.

When positioned for the IR band, the blue box 0.3-0.5  $\mu\text{m}$  provides the formation flying signal.

The formation flying alignment signal is the leaked Poisson spot from the star.

Example out-of-band guiding signal from HabEx report.

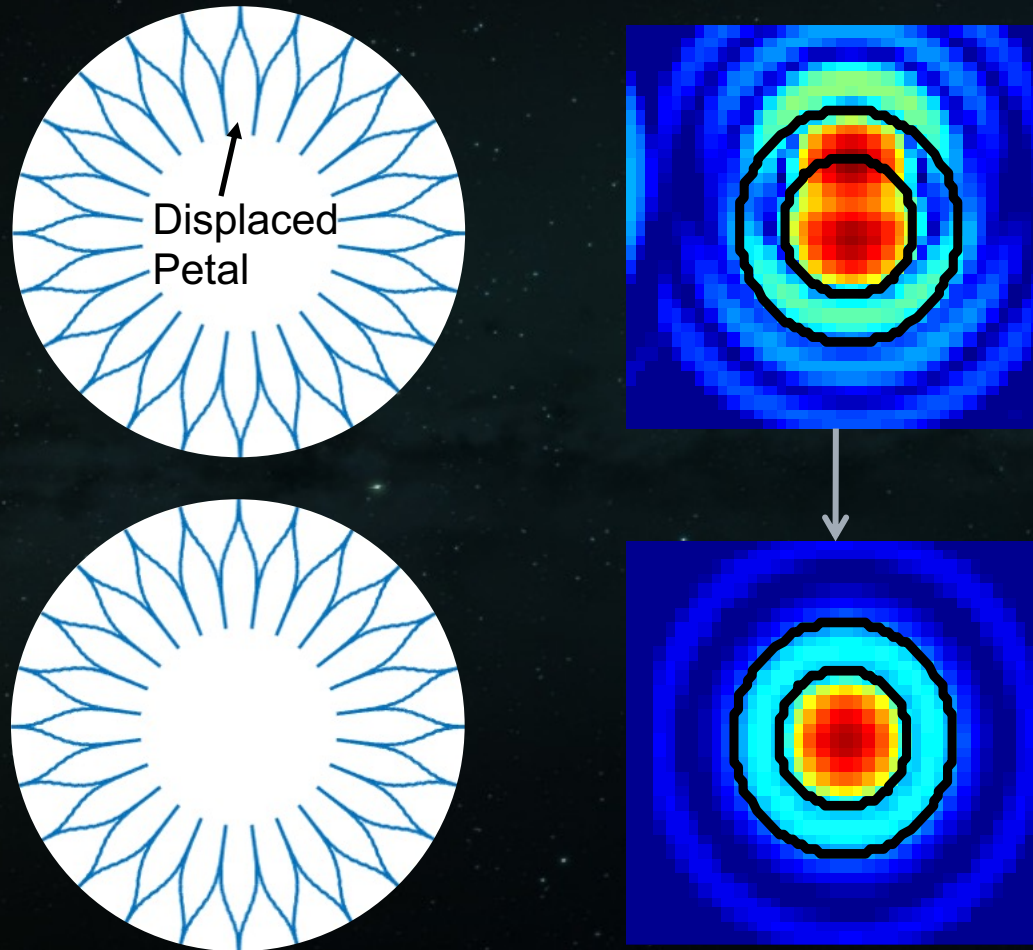


F080



# SPINNING

The starshade is spun about its axis at 12 revolutions per hour



- Benefits of spinning

- Reduce local thermal shape variations
- Circularize leakage from shape defects
  - **Speckles smear into annuli, not to be confused with an exoplanet.**
  - Relaxes deformation requirements: driven by photometric leakage rather than systematic leakage.
  - But does not eliminate localized solar glint and formation flying scatter
- No big reaction wheels
- Robust fault tolerance

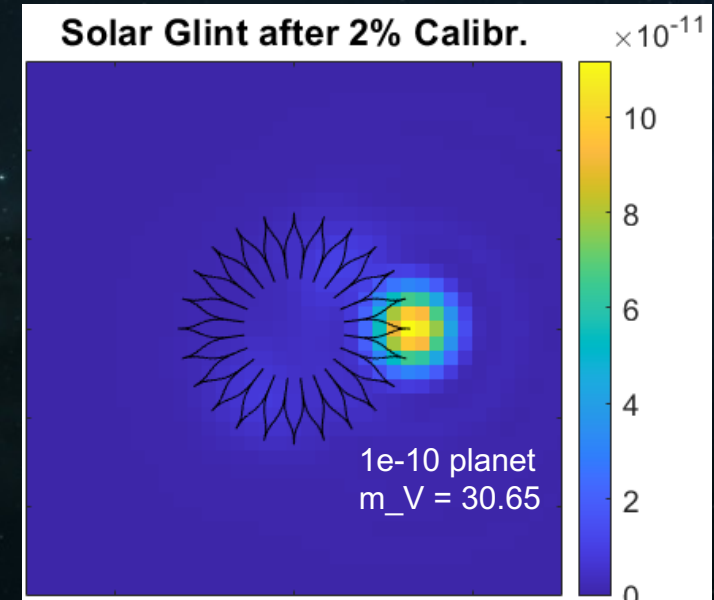
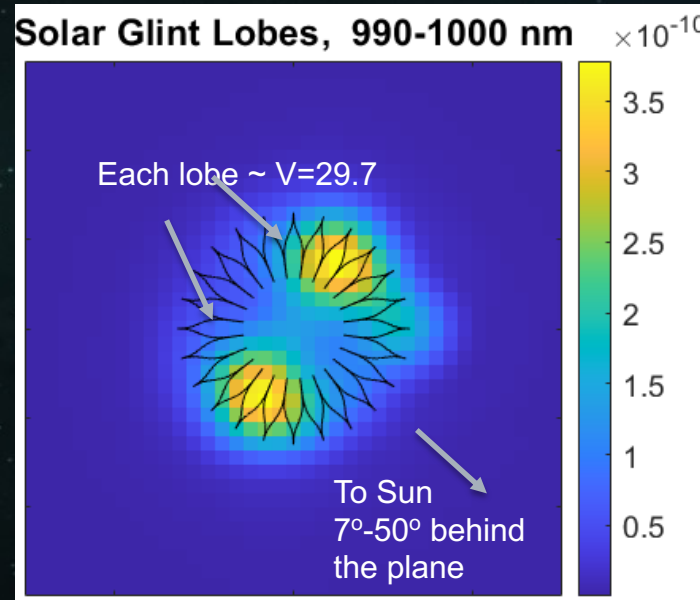
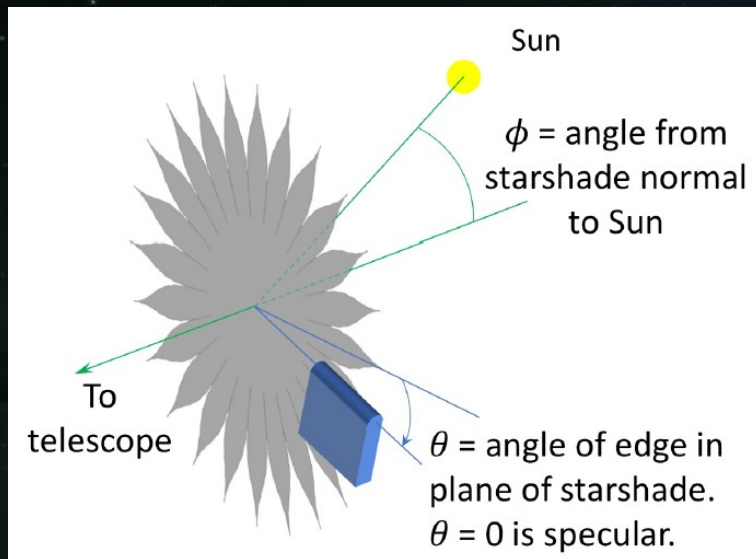
- Downside

- Requires some additional fuel to rotate the angular momentum vector

Spinning relaxes instrument calibration requirements.

# SOLAR GLINT LOBES: THE MAIN INSTRUMENT NOISE

The brightest contributors to instrument background near the IWA are the two solar glint lobes resulting from the Sun illuminating the edges of the starshade. Here we simulate imaging of a G4V  $V=5.65$  star.



The brightness of solar glint lobes is mitigated by employing sharp, anti-reflection coated edges. Highly accurate calibration is performed during initial on-orbit checkout by moving the starshade closer to the telescope.

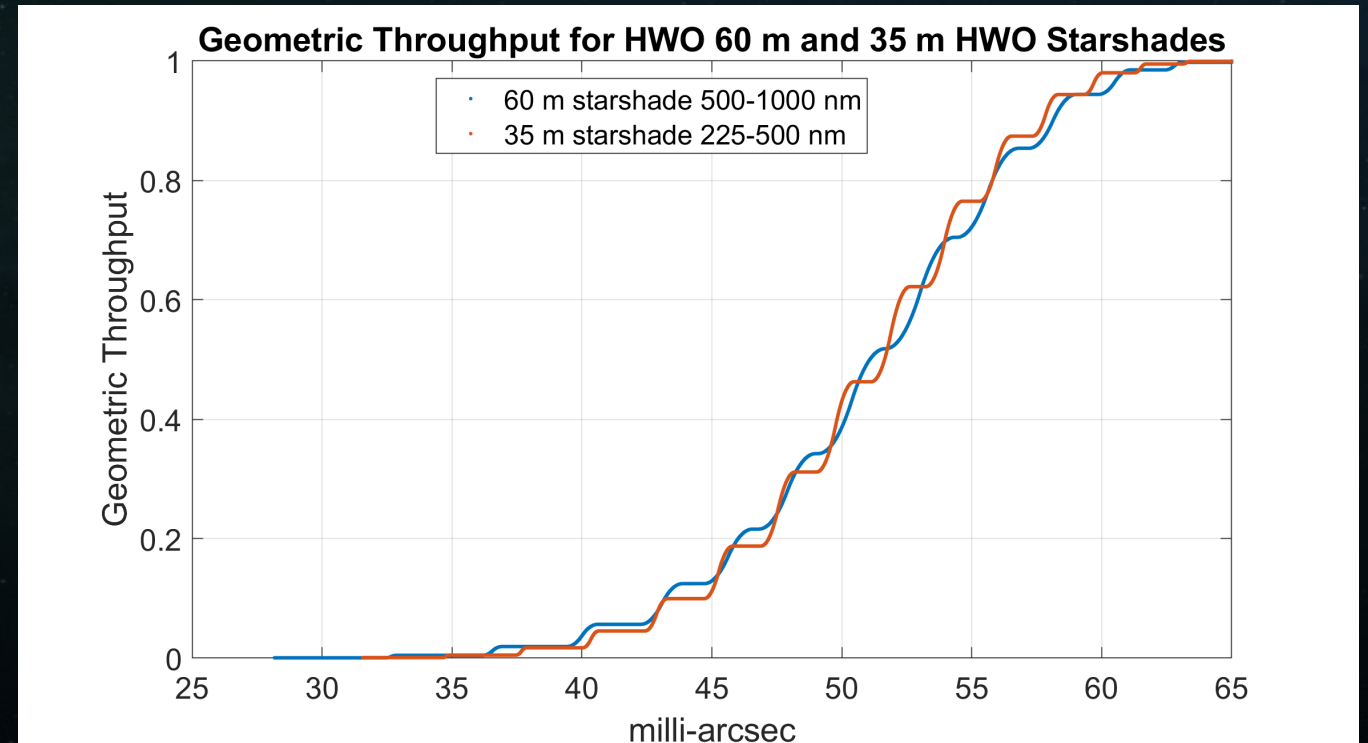
Solar glint lobes will have a visual magnitude of  $\sim 30$  averaged over the IWA.

# THROUGHPUT

Starshade throughput approximately follows the geometric opening of the petals (shown here). Instrument throughput is high because the cameras and spectrometers are relatively simple.

For exoplanet characterization, overall throughput is high due to a combination of:

- High starshade throughput
- High camera throughput
- Large instantaneous bandwidth
- Small calibration overhead

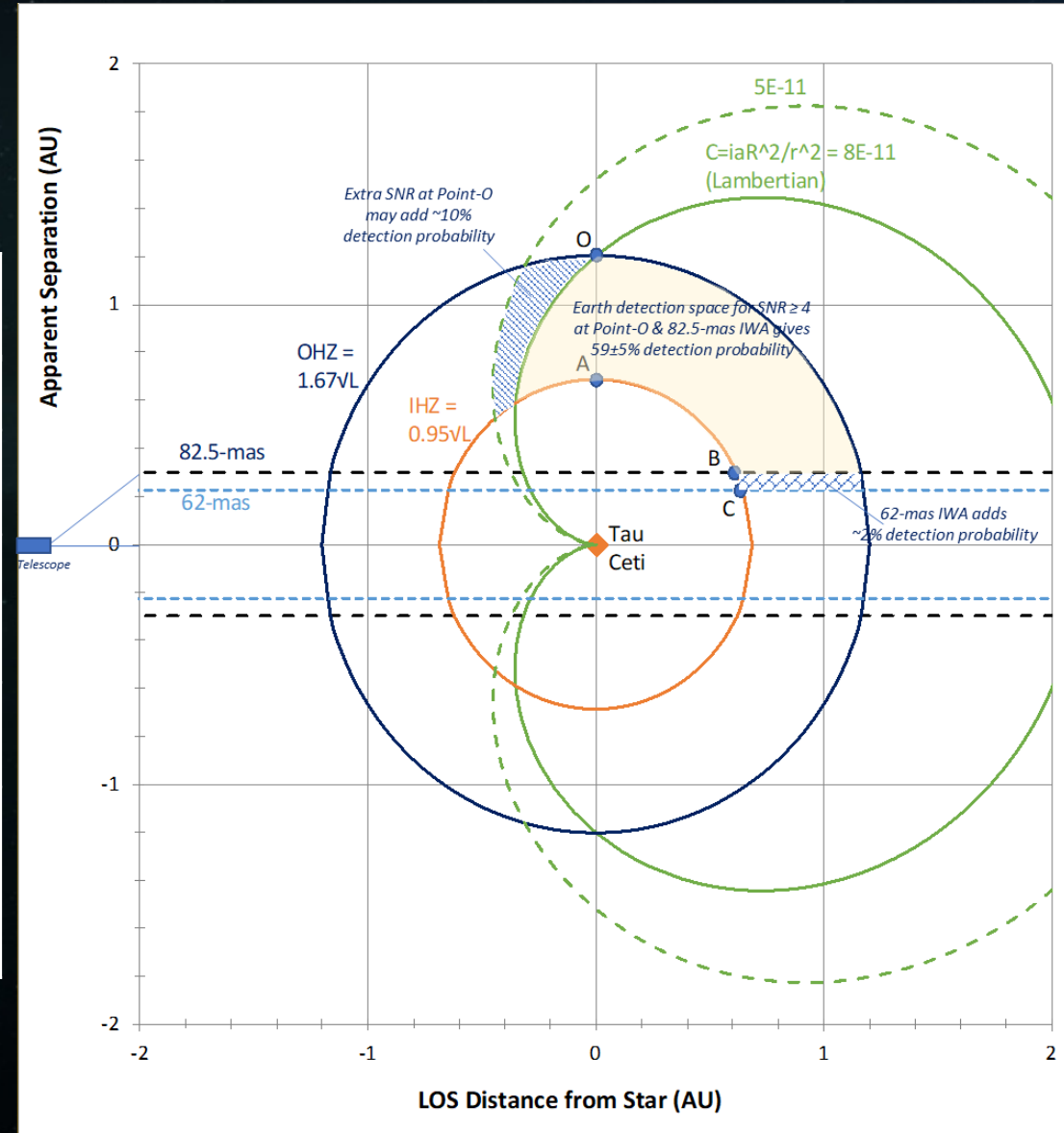




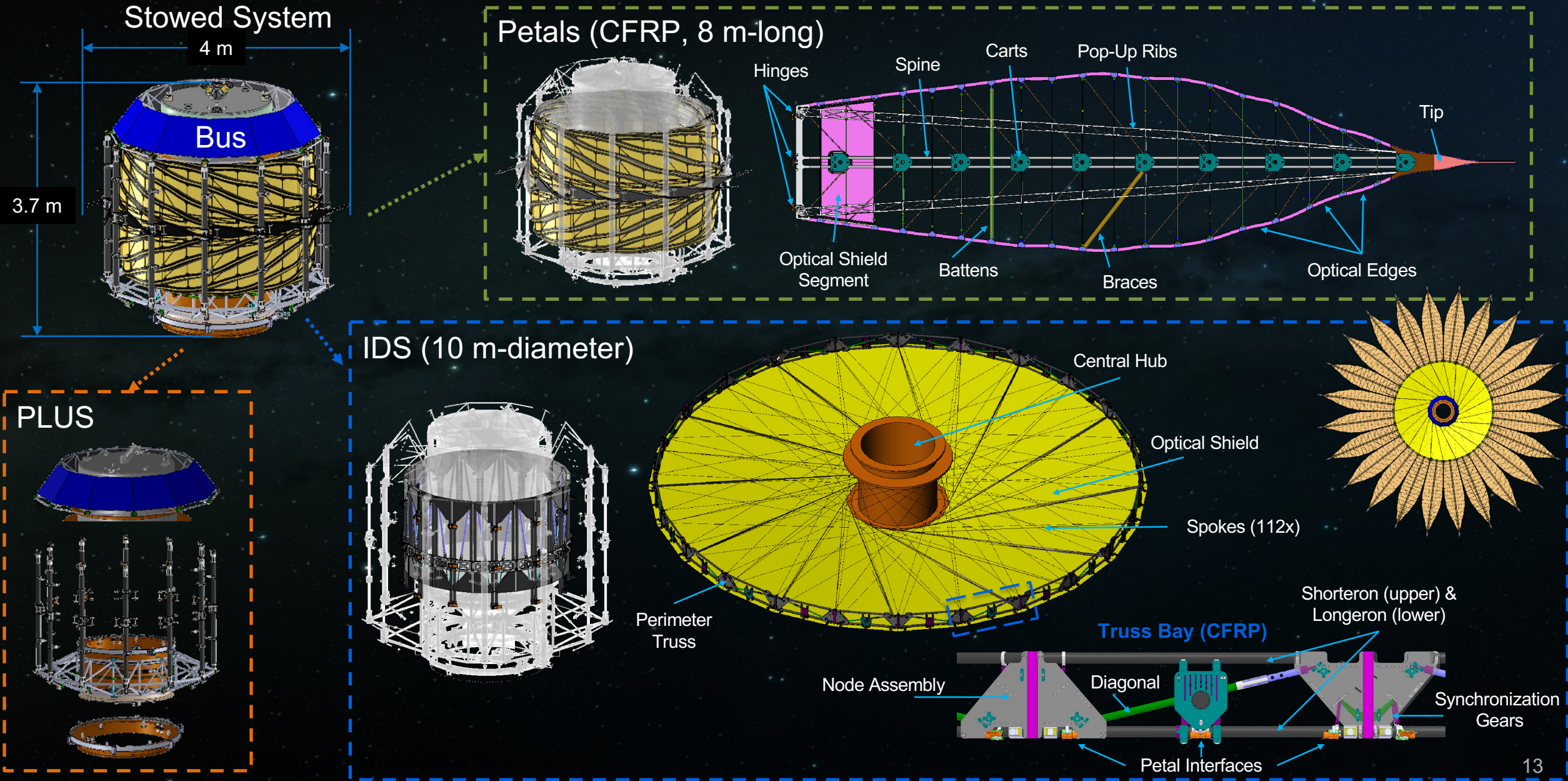
# OBSERVATIONAL COMPLETENESS

A starshade Design Reference Mission (DRM) favors a list of targets with high average observational completeness.

| Attributes for high-completeness per target               | What you gain   |
|---|---|
| Small IWA   | Access to IHZ   |
| Unlimited OWA, improving contrast with WA                 | Access to OHZ   |
| High throughput, wide bandwidth, low calibration overhead | Detected planets can be characterized before they disappear   |
| Weekly or slower cadence per target                       | Limited number of observations  |
| <b>NET RESULT</b>   | <b>Focus on fewer high-completeness stars.<br/>More access to early type stars.<br/>Higher success rate for revisits, e.g. orbit determination.</b> |

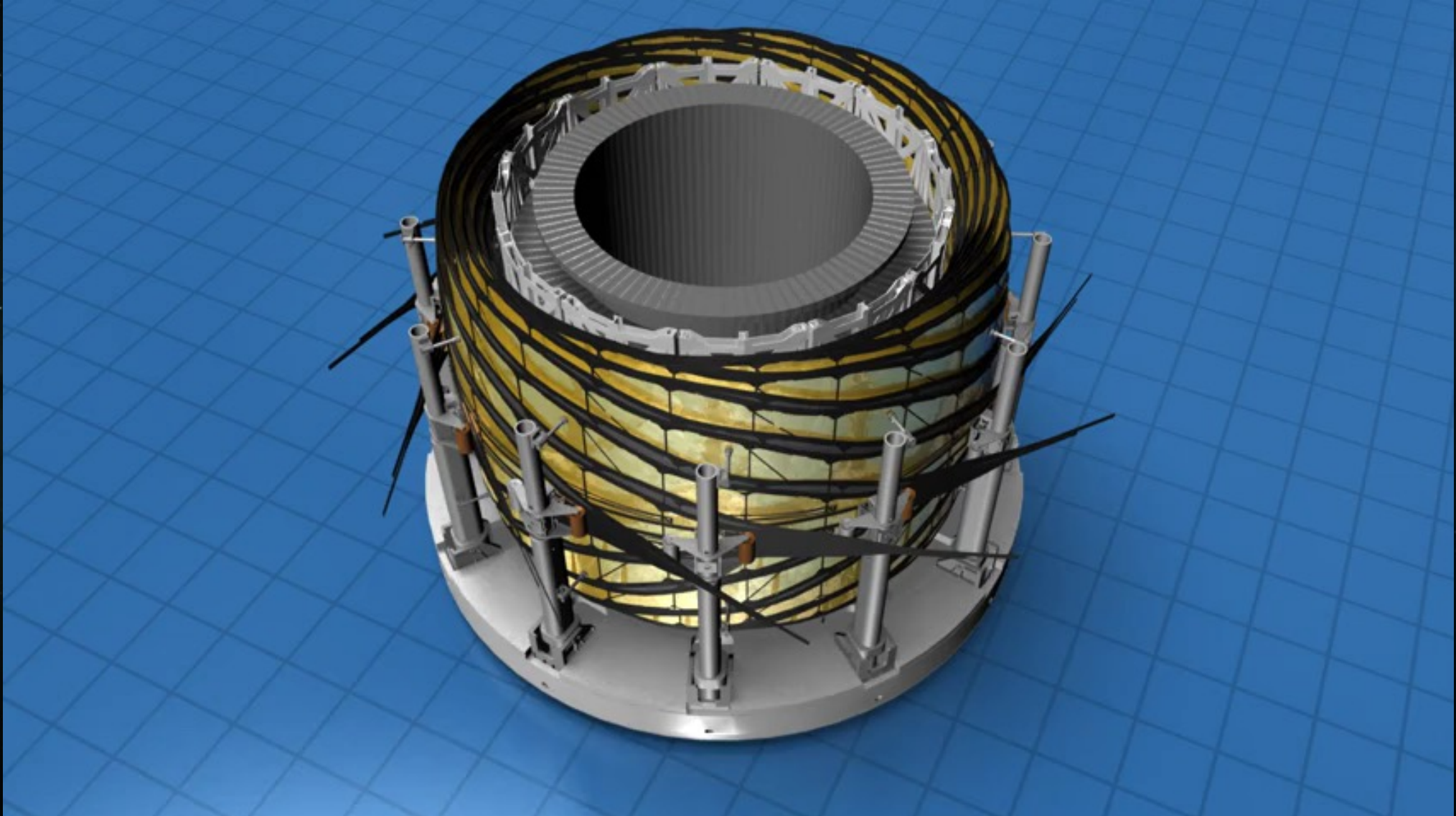


# STARSHADE CONFIGURATION





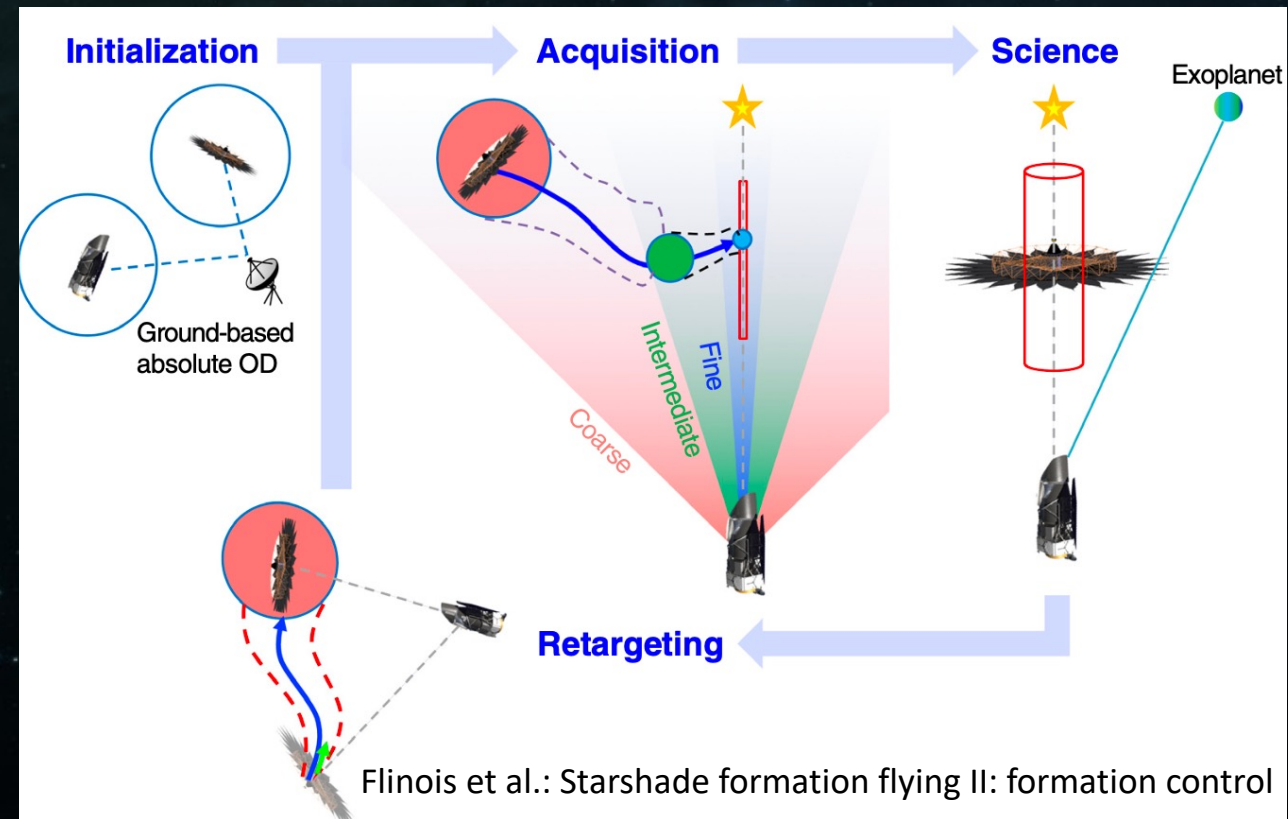
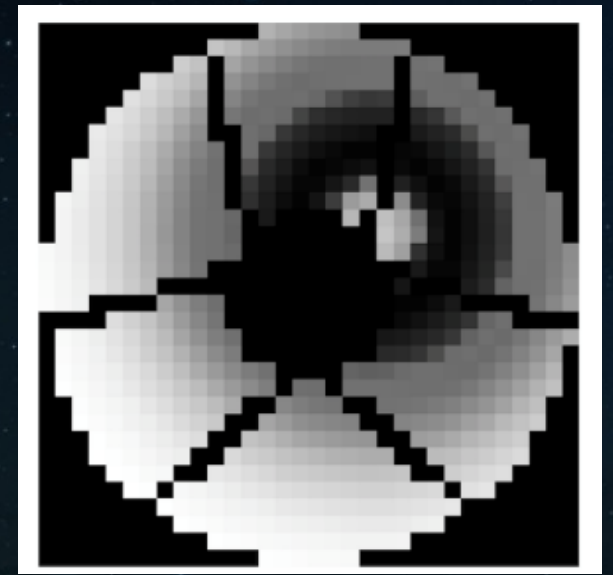
# STARSHADE DEPLOYMENT





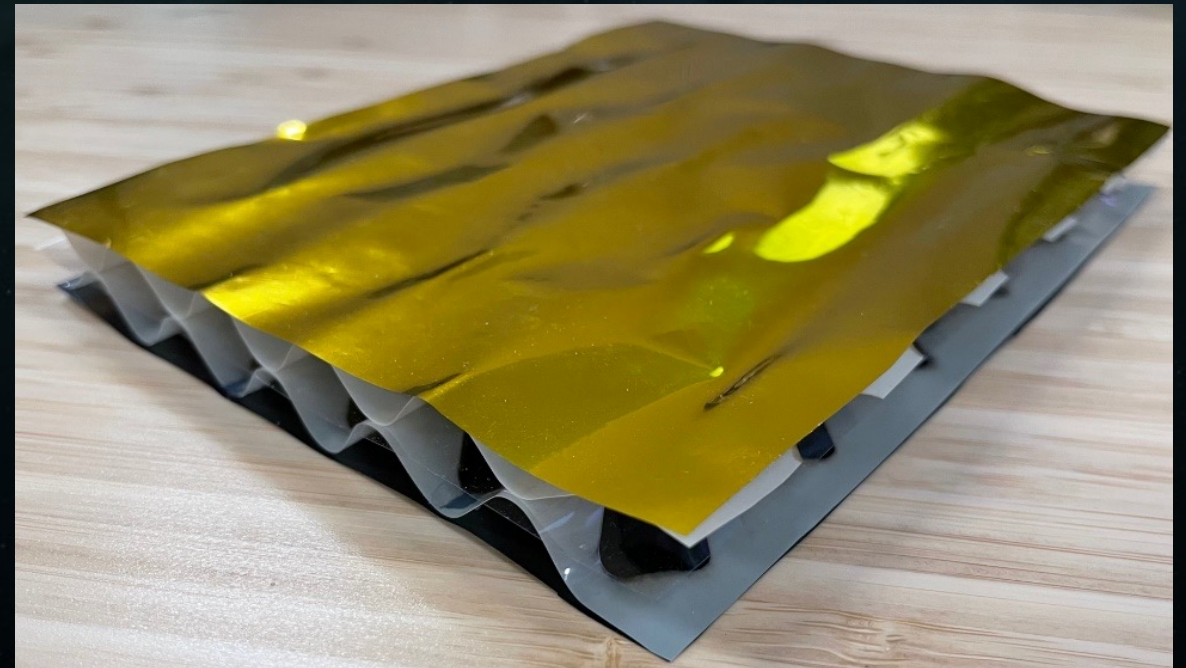
# FORMATION SENSING & CONTROL

- A starshade's lateral formation error is readily sensed in a telescope pupil-plane via its prominent Poisson Spot in out of band starlight
- A laser beacon on the starshade supports acquisition only
- A RF transponder relays the error to the starshade for control via biprop thrusters
- Low gravity gradients at E-S L2 & even less solar pressure give ~10-min. thruster firing periods, for a lateral control band of  $\pm 2\text{m}$  (i.e., 10-m dia. shadow)
- Potential detector saturation due to solar scatter from residual exhaust for ~10s can be avoided by reading out at a high rate
- Starshade sends thruster fire alerts via RF transponder
- Formation error contributes  $\leq 1\text{E-}11$  to instrument contrast



# MICROMETEOROIDS AND MISSION LIFETIME

- **An opaque optical shield mitigates micrometeoroids with multiple spaced layers**
  - Stops smaller highest flux particles
  - Requires many scattering reflections for **off-axis sunlight** to pass on-axis to the telescope
  - Limits solid angle for **on-axis starlight** to pass straight through without any scattering
- **HabEx study estimates provide useful HWO placeholders**
  - Off-axis sunlight  $\geq 31$  Vmag
  - On-axis starlight  $\leq 5E-12$  contrast
- **HWO's larger launch fairings/stowed volume allow more layers & greater layer separation to improve micrometeoroid stopping power**
- **A 10-yr. life may be viable, but requires a detailed design study**





# STARSHADE INSTRUMENT CONTRAST BUDGET



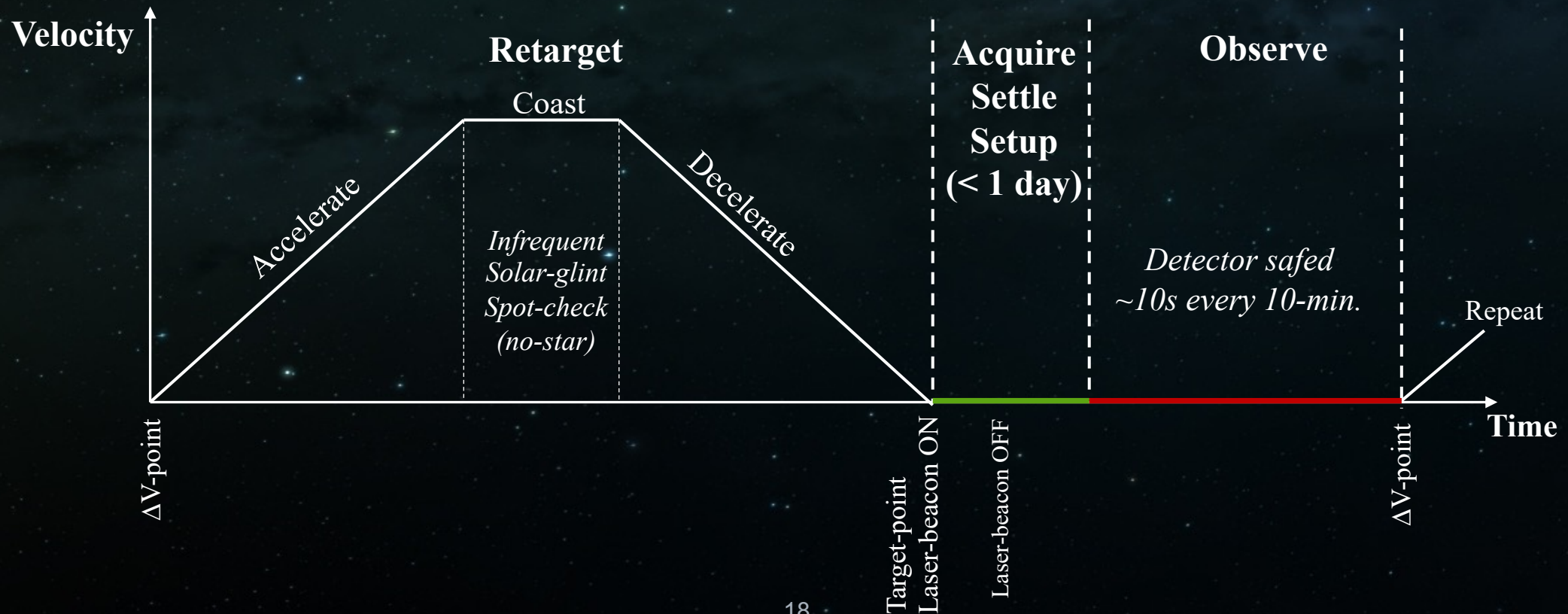
*Max expected contrast at  $3\sigma$ , or not to exceed levels that derive from S5 experiments & HWO simulations at  $1.9 \lambda/D$*

***The starshade limits instrument contrast to  $\leq 4E-11$  including large margins on top of max expected shape errors, demonstrated via ExoTAC approved technology milestones***



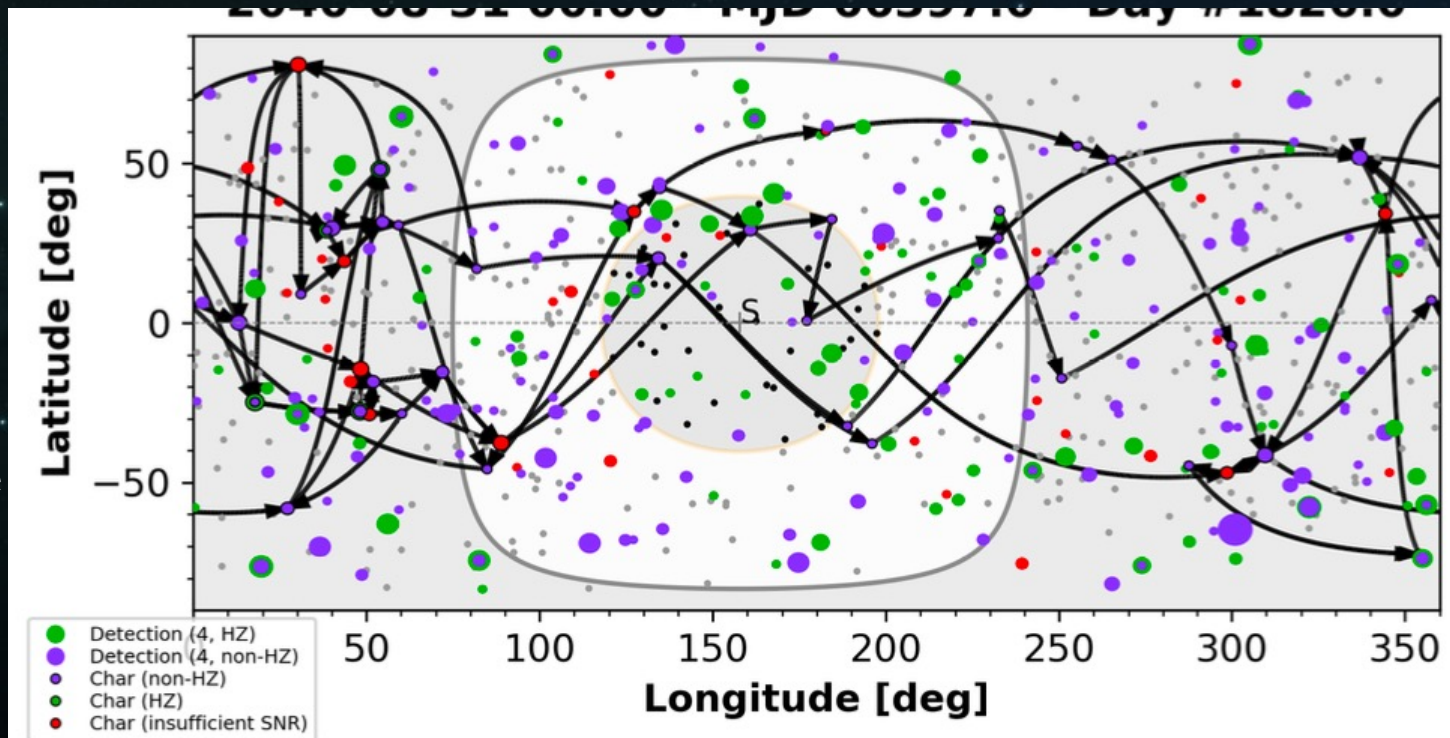
# OBSERVATION CADENCE

- Starshade observations always follow a retarget maneuver, to line up on the target, & an acquisition, which typically limits the encumbered telescope time to ~25%
- Observations are uninterrupted, except for ~10-s every ~10-min. for formation control thruster firings



# STARSHADE FIELD OF REGARD (FOR)

- Starshade observes  $\geq 40$  deg. (TBR) from Sun, to keep sunlight out of the telescope barrel
- Starshade observes  $\leq 83$  deg. from Sun, to avoid solar illumination of telescope-facing surfaces
- Target stars move through this FOR
- A typical avg. retarget slew rate of  $\sim 2$  deg/day gives an efficient observation sequence, keeping the starshade in the FOR



3-3. EXOSIMS design reference mission simulation scheduling observations planned for the broad and deep survey of the Starshade field of regard. Starshade retargeting transits over a nominal 5-year mission (2035–2040) are indicated by black arrows. Using realistic constraints such as solar field-of-regard, transit times and fuel usage, 100 starshade transits can be accommodated with fuel margins.



# STARSHADE RETARGET PERFORMANCE

- Retargets use Gateway's Hall Effect thruster with Xenon gas
  - Hall Effect Rocket with Magnetic Shielding (HERMeS)
  - 2,900-s specific impulse & 0.6-mN thrust, per engine
- PV cells on the starshade disk provide SEP power, with available disk area limiting total thrust
  - 35-m starshade powers 1 engine for 0.6-mN thrust
  - 60-m starshade powers 3 engines for 1.8-mN total thrust
- Starshades carry large propellant loads for significant science yield and refueling either augments the yield or adds a new mission phase
- A 35-m starshade is relatively agile & can blind-search ~150 stars in 4-years, then after refueling can revisit ~36 Earth candidates 4X each over 4 additional years
- Rhonda Morgan will next speak to 60-m starshade yield, sans refueling



*Hall-Effect thruster  
under test at JPL  
(In partial-vacuum)*

# STARSHADE CONCERNS

| Concerns, Risks, or Challenges  | Mitigations   |
|---|---|
| <p><b>Maintaining sufficient starshade cleanliness to limit solar scatter</b></p>   | <p>Clean-room assembly with shielding from gravity offload equipment<br/>           Deployed tests mostly with telescope facing surface pointed down<br/>           Stow within dry-N<sub>2</sub> purged container/thermal shroud<br/>           Remove before flight peel-off coating on optical edges</p> |
| <p><b>Optical performance demo. &amp; models validated only at subscale</b></p>   | <p>Ground tests match HWO mission petal Fresnel zones &amp; <math>n \lambda/D</math> IWA.<br/>           Future testbed of 3X length reduces polarization by 3X.</p>  |
| <p><b>Optical perf. demo. &amp; models validated only over part of band</b></p>   | <p>Ground tests match HWO mission petal Fresnel zones &amp; <math>n \lambda/D</math> IWA</p>  |
| <p><b>Refueling &amp; long mission makes micrometeoroids life-limiting</b></p>  | <p>Larger launch vehicle fairings allow more optical shield layers with greater layer spacing to greatly improve micrometeoroid stopping power</p>  |
| <p><b>Programmatic risk of a 60-m 1<sup>st</sup> starshade flight development</b><br/>           (large standing army cost)</p> | <p>Develop a high fidelity full-scale TRL-6 starshade system &amp; treat like flight, with noted exceptions</p>   |

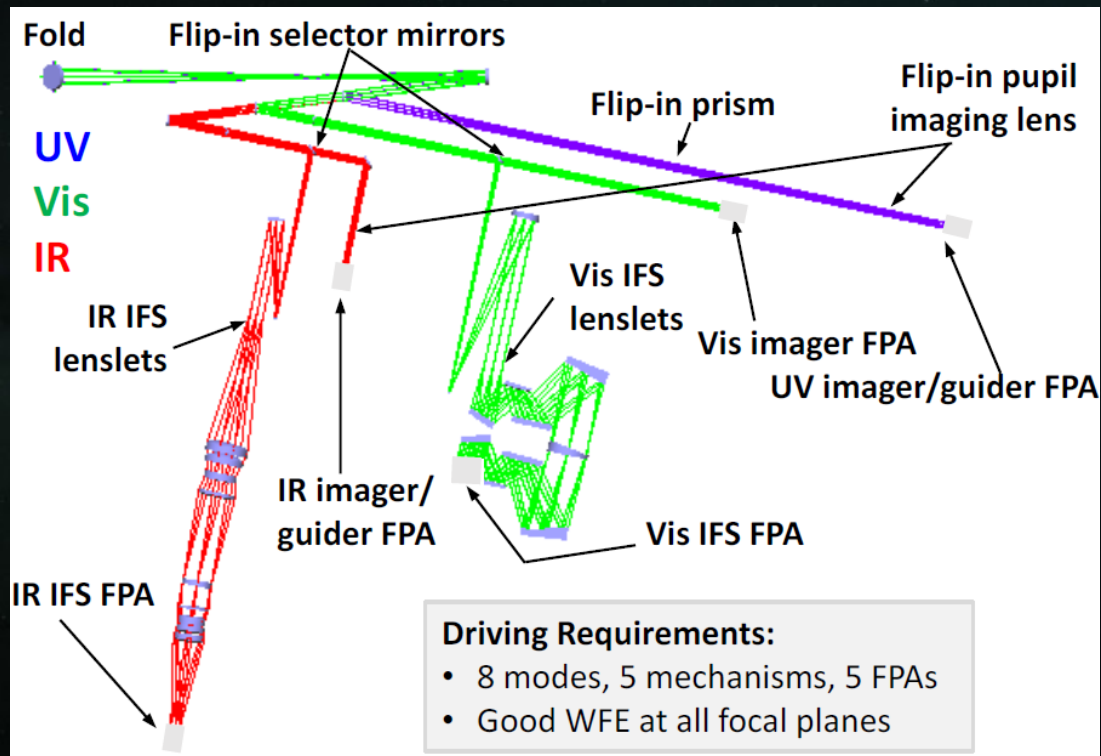


BACKUP

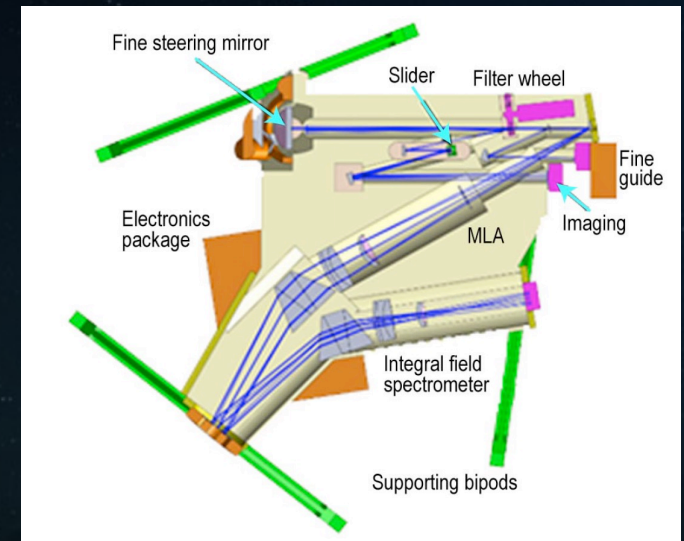
# CAMERAS

Starshade cameras and IFSs: Compact, High Throughput, Simple.  
Here are some examples:

A multi-band camera with IR and Vis IFS  
(Habex Lite 2018) IFS.



Exo-S Optical Instrument



A UV dedicated high-throughput camera with (O3 report).

